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# Processing a multifold ground penetration radar data using common-diffraction-surface stack method

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| Keywords   | Abstract   |  |  |  |
|--|--|--|--|--|
|  | Recently, the non-destructive methods have become of interest to the scientists in       |  |  |  |
| Ground Penetration   | various fields. One of these method is Ground Penetration Radar (GPR), which can         |  |  |  |
| Radar  | provide a valuable information from underground structures in a friendly environment     |  |  |  |
|  | and cost-effective way. To increase the signal-to-noise (S/N) ratio of the GPR data,     |  |  |  |
| CRS  | multi-fold acquisition is performed, and the Common-Mid-Points (CMPs) are acquire        |  |  |  |
|  | Compared to the traditional CMP method, which is applied to a CMP, the Common-           |  |  |  |
| CDS  | Reflection-Surface (CRS) method is introduced for seismic data processing considering    |  |  |  |
|  | the neighboring CMPs. In addition, instead of a point on the reflector, CRS assumes that |  |  |  |
|  | the reflector is part of a circle. With these two characteristics, CRS produces a stack  |  |  |  |
|  | section with a high S/N ratio. The Common-Diffraction-Surface (CDS) method, wh           |  |  |  |
| is a simplified version of CRS, enhances the diffractors related to the undergroup |  |  |  |  |
|  | anomalies like pipeline, flume, and caves. We apply the CDS stack method on a multi-     |  |  |  |
|  | fold GPR data and compare it to the CRS results. These results show that the CDS         |  |  |  |
|  | method can provide a high S/N ratio stack section compared to the traditional CMP        |  |  |  |
|  | method.  |  |  |  |

## 1. Introduction

Unlike the Common-Mid-Point (CMP) method, which assumes the horizontal underground reflector Dip-Move-Out (DMO) methods [1], which consider all dipping reflectors, the Common-Reflector-Surface (CRS) stack method is a generalized seismic data-processing that does not consider a point on a reflector but a part of a circle tangent to the reflector [2]. The CRS stack method is based on two hypothetical wave fronts so-called kinematic wave field attribute [3]. Based these attributes. the second-order on approximation of travel time has been developed. The travel time of the CRS operator is obtained by the paraxial ray theory [4, 5] or optic principle [6]. The CRS stack method in a full automatic manner was applied to a seismic data with very promising results [7, 8]. Afterwards an extension was added to the CRS method to handle the conflicting dip [9]. By merging the concept of DMO and CRS

methods, the Common-Diffraction-Surface (CDS) stack method was introduced in a data-driven manner so-called data-driven CDS [10-12]. The data-driven CDS method is computationally very expensive, and hence, the model-based CDS stack method has been introduced [13, 14]. The modelbased CDS method, which requires a velocity model with a minor accuracy, has been applied successfully to the synthetic and real seismic datasets [15]. The CDS operator enhances the diffractor and can image the reflectors with a reasonable aperture. As the geometry of the multi-fold GPR data is the same as the seismic data acquisition in 2D, and hence, it is possible to processes such a dataset by a seismic processing method like the CRS staking method [16]. Here, we applied the CDS stack method to a multi-fold GPR which dataset. was acquired for environmental studies for water content

evaluation in SW of Brazil. Then we compared the results obtained with the CRS stack sections.

#### 2. Theory

The CRS stack method is based on two hypothetical wave front experiments: one is related to an exploding point on the reflector so-called Normal-Incident-Point (NIP), which generates a NIP wave with the radius of  $R_{NIP}$  at the surface, and the second relates to an exploding surface on the reflector so-called normal wave, which generates an N wave with the radius of  $R_N$  at the surface (see Figure 1).

The emergence angle of these two waves is equal to alpha at the surface [3]. Based on these three parameters so-called kinematic wave field attributes, the hyperbolic approximation of travel time reads as:

$$t_{hyp}^{2} = \left(t_{0} + \frac{2\sin\alpha}{v_{0}}(x_{m} - x_{0})\right)^{2} + \frac{2t_{0}\cos^{2}\alpha}{v_{0}}\left(\frac{(x_{m} - x_{0})^{2}}{R_{N}} - \frac{h}{R_{NIP}}\right)$$
(1)

In this equation,  $\alpha$ ,  $R_{\text{NIP}}$ , and  $R_{\text{N}}$  are the kinematic wave field attributes,  $v_0$  is the surface wave velocity,  $x_m - x_0$  is the relative mid-point, and h is the half offset. The kinematic wave field attributes have to be calculated using the coherence analysis in multi-coverage dataset [18]. As the curvature of a point source is infinite for an underground diffractor, the radius  $R_{\text{N}}$  becomes equal to  $R_{\text{NIP}}$  at the surface for such a diffractor so-called  $R_{\text{CDS}}$ . Consequently, Equation (1) is simplified to:

$$t_{hyp}^{2} = \left(t_{0} + \frac{2\sin\alpha}{v_{0}}(x_{m} - x_{0})\right)^{2} + \frac{2t_{0}\cos^{2}\alpha}{v_{0}R_{CDS}}\left(\left(x_{m} - x_{0}\right)^{2} - h\right)$$
(2)

This equation can image the diffractor in to a full extent, and for the reflector in a reasonable aperture gives acceptable results. The unknown parameters in Equation (2) are  $\alpha$  and R<sub>CDS</sub>. Using the kinematic and dynamic ray tracings, it is possible to obtain R<sub>CDS</sub> for an arbitrary emergence angle  $\alpha$  in a velocity model with a minor accuracy [14]. For more details.



Figure 1. Two hypothetical wave fronts, one related to an exploding surface shown in blue that generates a wave front with a radius of  $R_N=1/K_N$  so-called the Normal (N) wave, and one related to an exploding point that generates a wave front with a radius of  $R_{NIP}=1/K_{NIP}$  at the surface so-called the Normal Incident Point (NIP) wave. Both waves emerge from the surface with the angel  $\alpha$  [17].

#### 3. Implementation

The seismic method is based on the measurements of the time that takes a mechanical wave that goes from the source to the receiver. The GPR method is basically the same. However, the GPR method deals with the electromagnetic wave instead of the mechanical wave. Hence, the total acquisition time and the sampling rate in the GPR data are in the order of nanoseconds. In addition, in a common survey for GPR data, the distance between the source and the receiver (offset) is constant along the profile, so called common offset array. By repeating the common offset array along a profile with a different constant offset, the multi-fold GPR dataset is obtained. The multi-fold GPR dataset is geometrically the same as the seismic 2D data set, i.e. time-CMP-offset. Consequently, it is possible to apply the new imaging methods like Common-Reflection-Surface (CRS) [7] or Common-Diffraction-Surface [12, 15] on such datasets, which have not been applied to the GPR dataset till now. In this work, we used the multi-fold GPR data, which acquired a Mala Geophysics Ramac-2 with 200-MHz antenna along a 55 m profile. The multi-fold GPR dataset is uncommon as it is acquired in one channel with a specific offset [16]. The specification of GPR acquisition is presented in Table 1.

The CRS stack method is applied to the multi-fold GPR data. The parameter that was used for the stacking process is shown in Table 2.

We applied the model-based CDS stack to this dataset with the parameters mentioned in Table 3 on a constant velocity model Vconst = 2800 m/s.

The stacked sections of CRS and CDS are shown in Figures 2 and 3, respectively.

| Table1. Data acquisition parameters.       |                        |  |  |  |
|--|------------------------|--|--|--|
| Title                                      | Amount                 |  |  |  |
| Shot interval                              | 0.1 m                  |  |  |  |
| Group interval                             | 0.2 m                  |  |  |  |
| Number of shots                            | 546                    |  |  |  |
| Number of active channels                  | 28                     |  |  |  |
| Number of total trace                      | 33840                  |  |  |  |
| Number of CMPs                             | 680                    |  |  |  |
| CMP distance                               | 25 m                   |  |  |  |
| Sampling interval                          | 1 ns                   |  |  |  |
| Number of sample per trace                 | 200                    |  |  |  |
| Number of total trace                      | 15302                  |  |  |  |
| Number of CMPs                             | 548                    |  |  |  |
| CMP distance                               | 25 m                   |  |  |  |
| First shot coordinate                      | (x=130  cm, y=0, z=0)  |  |  |  |
| Last shot coordinate                       | (x=5860  cm, y=0, z=0) |  |  |  |
| First geophone coordinate                  | (x=-190  cm, y=0, z=0) |  |  |  |
| Last geophone coordinate                   | (x=5530  cm, y=0, z=0) |  |  |  |
|  |                        |  |  |  |
| Table 2. Parameters used for CRS stacking. |                        |  |  |  |
| Parameter                                  | Amount Unit            |  |  |  |
| Surface velocity                           | 6000 cm/µs             |  |  |  |
| Mean frequency                             | 200 MHz                |  |  |  |
| mean nequency                              | 200 101112             |  |  |  |

| Surface velocity          | 6000  | cm/µs |
|---------------------------|-------|-------|
| Mean frequency            | 200   | MHz   |
| Minimum stacking velocity | 5500  | cm/µs |
| Maximum stacking velocity | 9500  | cm/µs |
| Minimum time              | 0.015 | S     |
| Maximum time              | 0.08  | S     |
| Minimum offset aperture   | 60    | cm    |
| Maximum offset aperture   | 600   | cm    |
| Minimum CMP aperture      | 100   | cm    |
| Maximum CMP aperture      | 20000 | cm    |

| Table 3. Parameters used for CDS | stacking. |
|----------------------------------|-----------|
|----------------------------------|-----------|

| Parameter                | Amount   | Unit   |
|--------------------------|----------|--------|
| Surface velocity         | 6000     | cm/µs  |
| Mean Frequency           | 200      | MHz    |
| Minimum time             | 0.0      | S      |
| Maximum Time             | 0.08     | S      |
| Minimum offset aperture  | 60       | cm     |
| Maximum offset aperture  | 600      | cm     |
| Minimum CMP aperture     | 100      | cm     |
| Maximum CMP aperture     | 100      | cm     |
| Range of Emergence angle | $\pm 40$ | degree |
| Allow turning rays       | No       | -      |



CRS stacked result Figure 2. The stacked section with CRS method.



Figure 3. The stacked section with model-based CDS stack method using a constant velocity model  $V_{const} = 2800$  m/s.

The continuity of the reflectors is preserved in the CDS stack section in Figure 3 compared to the CRS stack section shown in Figure 2. For instance, compare the reflector at time 50 ns and distance 7.5 m in Figures 2 and 3. In addition, the fractured points are well-imaged in CDS stacked section, while in the CRS stacked section, such fractions are missing. For example, compare the fraction at time 30 ns and distance 6 m in these two figures.

To have a better comparison, the two stack sections are compared. Figure 4 shows the windows 'A' to 'D' of the two stacked sections depicted in Figures 2 and 3.

As depicted in Figure 4a, processed by the CRS stack method, the continuity of the event is missing from times 20 µs to 110 µs and distance 2.5 m, while the counterpart stacked section, Figure 4b, processed by the CDS stack method, imaged this discontinuity very well. In Figure 4c, after the distance 11.7 m almost for all times, there are just the artifices, while in Figure 4d, all events are well-imaged. In addition, the discontinuities at 67 ns to 92 s at the distances 11.7 m and 14.8 m are clearly imaged. In Figure 4f, it is easy to follow the discontinuity at 58 µs to  $83 \ \mu s$  in distance 29.7 m, while this is not clear in Figure 4e. Finally, the events in Figure 4g are like artifices, although these events are smooth and continuous in Figure 4h. The CMP stack section of these datasets is depicted in Figure 5. With the comparison of this figure with the results of CRS and CDS staked section, illustrated in Figures 2 and 3, respectively, it is clearly obvious that the CMP stack method is very inefficient to image many of the events on stacked section.

Finally, comparisons between the frequency contents of the stacked section simulated by the CMP, CRS, and CDS stake methods have been shown in Figures 6a, 6b, and 6c, respectively. The

frequency content of the CMP stack section is contaminated by noise of high frequency from 17000 MHz to 30000 MHz. This high frequency disappears in CRS and CDS as these methods use the operator that consider a more number of traces. In addition, the high frequency events in Figure 6 with the frequency around 17000 MHz appear in all sections, which show that the CDS stacked section does not lost the high frequency events.



Figure 4. Comparison of four windows of Figures 2 and 3: a- Window 'A' in Figure 2, b- Window 'A' in Figure 3, c- Window 'B' in Figure 3, e-Window 'C' in Figure 2, f- Window 'C' in Figure 3, g- Window 'D' in Figure 2, h- Window 'D' in Figure 3.





CMP stacked result Figure 5. The stacked section with CMP method.



b)

Figure 6. The frequency content of the stacked sections: a) frequency content of the CMP stacked section, b) frequency content of the CRS stacked section, c) frequency content of the CDS stacked section.



Figure 6. Continued.

#### 4. Conclusions

The Common-Diffraction-Surface stack method, which is a simplification of Common-Diffraction-Surface stack, can simulate the Zero-Offset stack section with a high signal-to-noise ratio. In this work, we applied the CRS and CDS stack methods to multi-fold Ground Penetration Radar (GPR), which is not a common survey. The results obtained show that the stacked CDS sections of the continuity of the events are more preserve than the stacked CRS section. In addition, CDS can image the small fractions very well, while such fractions are missing in the CRS and CMP stacked sections. The frequency contents of the stacked sections for CRS and CDS are almost the same, which shows that the CDS method preserves the high frequency events.

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# پردازش دادهای رادار نفوذ زمینی چند پوششه با استفاده از روش برانبارش سطح پراش مشترک

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#### چکیدہ:

امروزه روشهای غیر مخرب مورد توجه زیاد دانشمندان قرار گرفته است. یکی از این روشها، روش رادار نفوذ زمینی میباشد. با استفاده از ایـن روش مـی تـوان اطلاعات بسیار با ارزشی را از ساختارهای زیرسطحی بدون تخریب محیطزیست و با هزینه اندک به دست آورد. به منظور افزایش نسبت سیگنال به نوفه این روش به صورت چند پوششه برداشت میشود و سپس آرایش نقطه میانی مشترک از دادهای برداشت شده استخراج میشود. در مقایسه با روش نقطه میانی مشترک که فقط بر روی یک گروه نقطه میانی مشترک پیاده سازی میشود، روش برانبارش سطح بازتاب مشترک که به منظور پردازش دادهای لرزهای توسعه داده شده است، چندین گروه نقطه میانی مشترک را در نظر می گیرد. علاوه بر این روش برانبارش سطح بازتاب مشترک که به منظور پردازش دادهای لرزهای توسعه داده شده است، منطبق بر بازتابنده است، در نظر می گیرد. این دو ویژگی باعث شده است تا این روش، مقاطع برانبارش شده با نسبت سیگنال به نوفه بالاتری نسبت به روشهای پیشین تولید کند. روش برانبارش سطح پراش مشترک که به نوعی ساده است تا این روش، مقاطع برانبارش شده با نسبت سیگنال به نوفه بالاتری نسبت به روشهای ناهنجاریهای زیرسطحی مانند خطوط لوله ها، قناتها و غارها را برجسته تر سازد. در پژوهش حاض روش برانبارش سطح پراش مشترک می می است می می از می می روی یک داده چنـد پوششه رادار نفوذ زمینی پیاده سازی شده است. این نتایج با خروجی روش سطح بازتاب مشترک می باشد، می توانـد پراش های مـر تبط بـا می می می روش برانبارش می توند می این می توی و غارها را برجسته تر سازد. در پژوهش حاض روش برانبارش سطح پراش مشترک می باشد می توانـد پراش هـای مـر تبط با موششه رادار نفوذ زمینی پیاده سازی شده است. این نتایج با خروجی روش سطح بازتاب مشترک و می می برانبارش مطح پراش مشترک مقایسه شده اند. نتایج نشـان

كلمات كليدى: رادار نفوذ زمينى، برانبارش سطح بازتاب مشترك، برانبارش سطح پراش مشترك.